

# LANDIS-II Dynamic Fire System Extension (v1.0) User Guide

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## Introduction

This document describes the Dynamic Fire System extension for the LANDIS-II model. For information about the model and its core concepts, see the *LANDIS-II Conceptual Model Description*.

### 1.1. Fire Occurrence

Fire starts are based upon the hierarchical fire frequency model of Yang et al. (2004) that divides fire occurrence into two separate events – fire ignition and fire initiation. A fire ignition is defined as the first instantaneous instance of a fire, caused by either natural or anthropogenic sources. Fire initiation is defined as the likelihood that a fire ignition will burn an entire cell, and is a probabilistic function of the fuel conditions of that cell.

At each time step, the number of fire ignitions is drawn for each fire regime unit from a Poisson distribution, with a parameter value  $\lambda$  defined by the user. The value of  $\lambda$  is equal to the average number of ignitions within the fire regime unit per time step. The number that is drawn from the distribution is the number of ignitions that will be attempted for that time step.

For each ignition, the fire module randomly selects a cell from the given fire regime unit, and evaluates whether the fire ignition initiates a fire event by comparing initiation probability of the fuel type present on that cell with a uniform random number:

$$\text{random}_{U(0,1)} \leq P_{\text{FuelType}} \rightarrow \text{fire event starts} \quad (\text{Eq. 1})$$

where  $P_{\text{FuelType}}$  is a user-defined parameter between 0 and 1 (default = 1) defined for each fuel type.

### 1.2. Event Size

The fire module determines individual fire sizes and shapes using spread equations adapted from the Canadian Forest Fire Behavior Prediction System (FBP; Forestry Canada Fire Danger Group 1992) and an adaptation of the minimum travel time method described by Finney (2002), combined with a predetermined fire size or duration defined in Section 2.3. The fire spread algorithm entails two components: wind bias, and fuel-based spread. The wind bias component assumes an ellipsoidal shape with dimensions (i.e., length, breadth) dependent on wind speed. The fuel-based spread component is determined by a combination of fuel class (derived from a fuel module), wind strength, and topography. The wind bias and fuel-based spread combine to calculate the total spread rate, which incorporates fuel class, wind speed, wind direction, topography and the location of the pixel relative to the source pixel. The inverse of the spread rate is used as a cost surface to calculate minimum travel time to cross each pixel. The cumulative minimum travel time determines the final shape of an individual fire patch based on a cutoff determined by either a predetermined fire size or duration.

This fire module has two options for controlling the size of a fire for a given fire event: size-based and duration based. Former versions of LANDIS used a size-based option,

i.e., once a fire was initiated, a fire size was randomly selected from a user-defined lognormal distribution, and the fire spread until it either reached that size or ran out of cells that can burn (He and Mladenoff 1999). When the size-based option is applied in this fire module, burned sites are selected in order of increasing minimum cumulative travel time until the number of sites selected multiplied by the cell area equals or exceeds the predetermined fire size.

Alternatively, this fire module can randomly select a fire *duration* from a user-defined distribution, an approach first applied within Fin-LANDIS (Pennanen and Kuulaivanen 2002) that allows the fire regime (i.e., fire size distribution and fire rotation) to be influenced by the landscape configuration of fuels. When the duration-based option is applied in this fire module, all sites with a minimum cumulative travel time that is less than or equal to the predetermined fire duration are selected to become the burned area for that individual fire event.

Both fire sizes and fire durations are assumed to follow a lognormal distribution, with parameters  $\mu$  (Mean Fire Size: MFS; or Mean Fire Duration: MFD),  $\sigma^2$  (Standard Deviation of Fire Size: SDS; or Standard Deviation of Fire Duration: SDD), and maximum (size or duration) to simulate fire spread. Minimum size or duration is assumed to be zero. Size units are in hectares, and duration units are in minutes. The above distributions can be parameterized independently for each fire regime unit.

When a fire size or duration is selected, a size or duration class is assigned to the event based on the likelihood of that size or duration being selected from the distribution. Five size/duration bins are defined by the percentiles listed below (Table 1; from MN DNR). The size/duration class is used to link fire size or duration to fire weather (Section 1.3)

Table 1. Fire size/duration classes based on percentiles.

Description	Class	Probability	Percentile
Extreme	5	2.5%	97.5
Very High	4	7.5%	90
High	3	13.5%	76.5
Moderate	2	30%	46.5
Low	1	46.5%	0

### 1.3. Fire Event Weather

In this fire extension, the weather associated with a fire event is assumed to be related to the size or duration of the fire. This follows the general assumption that larger and longer duration fires tend to occur when fire weather is more favorable for burning, and smaller and shorter duration fires occur when fire weather is unfavorable. This link between size/duration and fire event weather is done by assigning both fire size/duration and weather records to classes based on their frequency. The fire size/duration classes are described above (Section 1.2), and the weather classes are described below.

The fire module requires the following weather input: season (spring, summer, fall), leaf status (leaf-on, leaf-off), wind speed velocity (WSV) in km per hour, wind direction

(WDIR) in degrees, fine fuel moisture code (FFMC), the Buildup Index (BUI), and the percent curing. FFMC and BUI are indices calculated as part of the Canadian Forest Fire Weather Index System (Van Wagner 1987). Fire weather inputs are provided by the user in a database defined in the parameter file. The current version defines the weather conditions to be constant for the entire event. Users can allow the fire weather distributions to change over time throughout the simulation by using different databases at different time steps.

For each season, representative daily values of WSV, FFMC, BUI, and WDIR are required for each fire region. These components are supplied as a table of daily weather records for each season within a Microsoft Access database. The database should contain tables named for each season (“region1\_Spring”, “region2\_Summer”, “region3\_Fall”, etc.). Season names should be capitalized, and fire region names should match those listed in the fire region table (see Section 2.5) exactly (capitalization matters). Each table should contain fields labeled “FFMC” (Fine Fuel Moisture Code), “BUI” (Build-Up Index), “WSV” (Wind Speed Velocity), and “WindDir” (Wind Direction). Each row should represent a daily record of weather data representative of the specified fire region. FFMC, BUI, WSV, and WindDir fields must have the DataType set to Number, with FieldSize set to Double.

In addition to the WSV, FFMC, BUI, and WDIR, each record should contain a field labeled “FWIBin”, which identifies the class (1-5) used to link the weather records to size/duration classes. Class 5 should include weather records with the most extreme fire weather, and Class 1 should include records with the least favorable fire weather. Users can assign the classes in any manner, though the original intent was to use the Fire Weather Index (FWI) as a means for ranking. FWI can be calculated using WSV, FFMC, and BUI (Van Wagner 1987). The percentiles in Table 1 above can be used to put weather records into classes based on FWI values. A table with at least 1 record in each FWIBin is required for any season that has a fire ignition rate (Section 1.1) greater than zero.

The text file that provides the weather data can change during the course of the simulation. This allows users to have different weather distributions represented at different times. This option is useful for modeling climate change scenarios.

### 1.3.1. Season

The fire module selects the season for a fire event based on the proportion of fires that occur within each season, defined by the user. The selection of season defines the leaf status for the fire event. By default, spring and fall seasons are considered leaf-off, and summer is considered leaf-on. These values can be changed by the user.

### 1.3.2. WSV, FFMC, BUI, WDIR

The fire extension selects the wind speed velocity (WSV), fine fuel moisture code (FFMC), buildup index (BUI), and wind direction (WDIR) for a fire event based on daily weather records supplied by the user. For each of the season-fire region combinations (spring, summer, fall for each fire region), the

user defines a table of daily weather. After the fire size/duration has been selected for the event, the program randomly selects a record from the appropriate fire region-season table that have specific fire weather classes (FWIBin) relative to the assigned size/duration class. Which FWIBins can be selected is controlled using the optional Weather Randomizer. The default weather randomizer (0) allows only the exact corresponding FWIBin (same bin value as selected size/duration bin) to be selected. Larger values for the weather randomizer (up to 4) allow the selection of weather records from additional adjacent weather bins. A weather randomizer value of 4 completely eliminates the link between fire size/duration bins and FWIBins. The values for WSV, FFMC, BUI, and WDIR for the event are read from the selected record.

Wind Direction Note: The value for wind direction in this extension should be considered carefully. Normally, wind direction reported from weather stations is the direction that the wind is coming *from*. In all calculations in this extension, we require the direction that the wind is blowing *to*. Therefore, the weather station wind directions may need to be adjusted by 180 degrees before calculating wind direction probabilities.

### 1.3.3. Weather Effects: Initial Spread Index

**Equation numbers in parentheses preceded by “FBP” refer to the corresponding equation numbers in Forestry Canada Fire Danger Group (1992).** Spread rate calculations begin with initial spread index (ISI) based on Van Wagner (1987):

$$ISI = 0.208 \times f(W) \times f(F) \quad (\text{FBP}; 52)$$

where the fuel moisture effect  $f(F)$  is:

$$f(F) = 91.9 \times e^{(-0.1386 \times m)} \times \left[ 1 + \frac{m^{5.31}}{4.93 \times 10^7} \right] \quad (\text{FBP}; 45)$$

$$m = \frac{147.2 \times (101 - FFMC)}{59.5 + FFMC} \quad (\text{FBP}; 46)$$

The wind effect  $f(W)$  is:

$$f(W) = e^{0.05039 \times WSV} \quad (\text{FBP}; 53)$$

Where WSV exceeds 40 km/hr:

$$f(W) = 12 \times \left[ 1 - e^{-0.0818 \times (WSV - 28)} \right] \quad (\text{FBP}; 53a)$$

## 1.4. Rate of Spread

The combination of fuel type, wind strength, fuel moisture conditions, and (optionally) topography determines the fuel-based spread component. The fuel type is determined through the separate fuel extension (Dynamic Fuel System extension), which evaluates species/age composition to assign fuels to user-defined fuel types. The fuel type-specific

rates of spread are calculated using equations from the Canadian FBP (Forestry Canada Fire Danger Group 1992), although users can alter input parameters to accommodate any fuel type.

Each user-defined fuel type (see Section 2.15) identifies a base fuel type (conifer, deciduous, conifer plantation, slash, open) and a surface fuel type (C-1 to C-7, D-1, S-1 to S-3, O-1a, O-1b) which define the fire behavior of each fuel type. Users are free to adjust inputs. For simplicity in this users guide, we will address fuels as if they match directly with Canadian FBP types, though the same logic and equations apply to other fuel types. For example, when we address fuel type C-1, the referenced equations will apply to any fuel type that has a surface fuel type defined as C-1.

The Dynamic Fire extension currently assumes that fires instantly reach equilibrium rates of spread. Future versions of the extension might account for acceleration and deceleration periods affecting fire spread (i.e., Equations 70-73; Forestry Canada Fire Danger Group 1992). However, they are not implemented here.

#### 1.4.1. Fuel Effects on Spread Rate

For conifer fuel types (C-1 to C-7), leafless deciduous (D-1), and slash (S-1, S-2, and S-3), the initial rate of spread (RSI):

$$RSI = a \times [1 - e^{(-b \times ISI)}]^c \quad (\text{FBP; 26})$$

where  $a$ ,  $b$ ,  $c$  are fuel type-specific coefficients listed in the Fuel Type Table (see section 2.15). Leaf-on deciduous is assumed to be 20% of leaf-off spread rates.

For mixed conifer-deciduous, the rate of spread is assumed to be a blend of a conifer type (C-1 to C-7) and D-1. For M-1 (leaf-off):

$$RSI = \left[ \frac{PC}{100} \times (RSI_{C-\#}) \right] + \left[ \frac{PH}{100} \times (RSI_{D-1}) \right] \quad (\text{FBP; 27})$$

Where PC = percent conifer and PH = percent hardwood. The FBP equations for M-1 and M-2 use only the conifer type C-2. In this extension, we allow the mixing of any conifer type in the M-1 and M-2 fuel types.

For Fuel Type M-2 (leaf-on), apply the same assumption that the deciduous component will burn at 20% of the leaf-off spread rate:

$$RSI = \left[ \frac{PC}{100} \times (RSI_{C-\#}) \right] + 0.2 \times \left[ \frac{PH}{100} \times (RSI_{D-1}) \right] \quad (\text{FBP; 28})$$

For fuel type M-3 (dead balsam fir mixedwood leaf-off), calculate coefficients as:

$$a = 170 \times e^{\left(\frac{-35}{PDF}\right)} \quad (\text{FBP; 29})$$

$$b = 0.082 \times e^{\left(\frac{-36}{PDF}\right)} \quad (\text{FBP; 30})$$

$$c = 1.698 - 0.00303 \times PDF \quad (\text{FBP; 31})$$

Where PDF = percent dead fir (or other conifers). PDF is calculated by the fuel extension based on the number of dead conifer cohorts, which is provided by the BDA or other disturbance extension.

For fuel type M-4 (dead balsam fir mixedwood leaf-on), calculate coefficients as:

$$a = 170 \times e^{\left(\frac{-35}{PDF}\right)} \quad (\text{FBP; 32})$$

$$b = 0.0404 \quad (\text{FBP; 33})$$

$$c = 3.02 \times e^{(-0.00714 \times PDF)} \quad (\text{FBP; 34})$$

The rate of spread in Open Fuel Types (O-1a, O-1b) is dependent on the degree of curing (i.e., the percentage of dried stems):

$$CF = 0.02 \times C - 1.0 \quad C > 50 \quad (\text{FBP; 35})$$

where CF is the grass curing coefficient and C is the degree of curing (%). When  $C \leq 50$ ,  $CF = 0$ . Hence the initial rate of spread for Open Fuel Types is:

$$RSI = a \times \left(1 - e^{-b \times ISI}\right)^c \times CF \quad (\text{FBP; 36})$$

CF is determined by season based on the user input (see Section 2.11).

Note: The above equations, in combination with the season of burn, and some assumptions regarding the curing coefficient, give users the opportunity to capture the essence of wetland burn rates (i.e., wetlands will only burn when drawdown is sufficient to dry surface material – much more likely in late summer/fall).

#### 1.4.2. Fuel Moisture Build-up Index

A buildup index (BUI) modifies spread rates to account for longer weather time lags than FFMC (i.e., 10-day time lag). The use of BUI to influence rate of spread is optional (see Section 2.5). The influence of BUI on rate of spread is dependent on the fuel type, and is expressed as the buildup effect (BE):

$$BE = e^{\left[50 \times \ln(q) \times \left(\frac{1}{BUI} - \frac{1}{BUI_0}\right)\right]} \quad (\text{FBP; 54})$$

BUI is the weather-derived Build Up Index (see Section 1.3.2);  $BUI_0$  is the average BUI for the particular fuel type from the Fuel Type Table (Section 2.15).

Rate of spread can then be calculated for all types except C-6 as the following:

$$ROS = RSI \times BE \quad (\text{FBP; 55})$$

Conifer Plantations (Fuel Type C-6): Rate of spread (ROS) equations for conifer plantations are different than other fuel types following the calculation of RSI. For C-6 fuels:

$$RSS = RSI \times BE \quad (\text{FBP; 63})$$

where RSS is the surface fire rate of spread.

$$RSC = 60 \times \left(1 - e^{-0.0497 \times ISI}\right) \times \frac{FME}{FME_{avg}} \quad (\text{FBP; 64})$$

$$FME = \left( \frac{[1.5 - 0.00275 \times FMC]^4}{460 + [25.9 \times FMC]} \right) \times 1000 \quad (\text{FBP; 61})$$

where  $FME_{avg}$  is 0.778, and FMC is foliar moisture code (see Section 1.8, Fire Severity).

$$ROS = RSS + CFB \times (RSC - RSS) \quad (\text{FBP; 65})$$

where CFB is crown fraction burned (see Section 1.8, Fire Severity). ROS is equivalent to the rate of spread (m/min) if the site is directly downwind from the source cell.

### 1.4.3. Fire Region Adjustment

Because fire regimes are parameterized independently for each fire region, it is possible for fires starting in one fire region to spread into another. This can affect the integrity of the individual fire regimes. The fire size distribution of the fire region can be preserved by altering the spread rates according to the mean fire size or duration of the unit where the fire started. To do so, a Fire Regime Unit Adjustment (*FRUA*) is calculated (**a fire regime unit is equivalent to a fire region**).

For a size-based fire regime:

$$FRUA_i = \frac{MFS_i}{MFS_{init}}$$

For a duration-based fire regime:

$$FRUA_i = \frac{MFD_i}{MFD_{init}}$$

For that particular fire event, rates of spread for each cell in fire region *i* are recalculated as:

$$ROS_i = ROS \times FRUA_i$$

This adjustment will cause fires to burn relatively more area within fire prone regions than fire resistant regions for a given fire event. However, the original spread rates will be used to calculate fire severity (see Section 3).

## 1.5. Fire Burned Area

The burned area for a fire event is determined by selecting cells based on the time it would take the fire to reach each cell from the ignition (i.e., minimum travel time). The total travel time is calculated starting from the ignition location. The program calculates the travel time to each active neighbor cell (8 cells maximum), and chooses the cell with the lowest cumulative travel time. The program then treats that chosen cell as the fire source and calculates the travel time to each of its active neighbor cells, and chooses the cell with the lowest cumulative travel time. This process continues until the cumulative

travel time exceeds the selected event duration or the number of cells checked exceeds the selected event size. The program repeats this process multiple times to ensure that the chosen spread sequence results in the calculation of the actual minimum travel times for each cell.

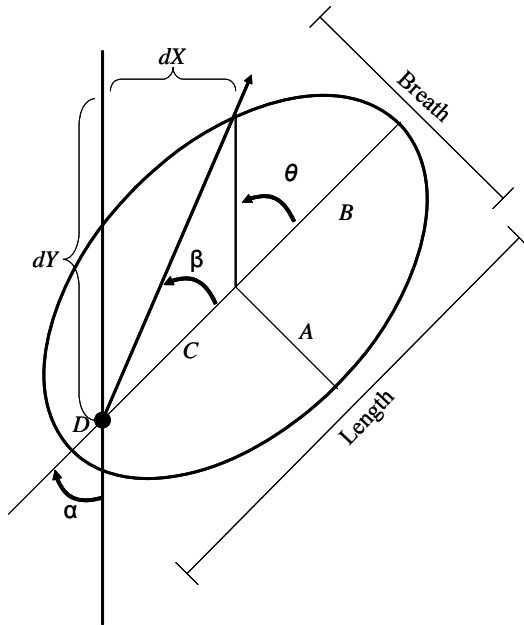


Figure 1. Main features of a fire ellipse (adapted from Finney 2002).

### 1.5.1. Fire Burned Area: Calculating Spread Rate for Each Cell

Fire spread is limited to each cell's 8 adjacent neighbor cells. The cell that the fire is spreading from is the source cell (beginning with the initiation site), and the cell that the fire is spreading to is the target cell. Calculating actual rates of spread begins with  $\beta$ , the angle formed between the wind direction ( $\alpha$ ) and the line between the source and target cells (see Figure 1).

$$\beta = \tan^{-1}\left(\frac{dX}{dY}\right) - \alpha \quad (\text{Finney 2002; Eq. 4})$$

where  $dX$  is the difference in row numbers between the source cell and the target cell;  $dY$  is the difference in column numbers. Note: if  $dY$  is less than zero, add 180 to  $\beta$ . To reduce artifacts of shape that can occur with the limitation of spreading to only 8 neighbors, the  $\beta$  angle is stochastically varied within a range of  $\pm 22.5$  degrees.

The length-to-breadth ratio (LB) for the fire event ellipse is determined by the selected WSV for the event.

For all fuel types except O-1:

$$LB = 1.0 + 8.729 \times \left[1 - e^{-0.030 \times WSV}\right]^{2.155} \quad (\text{FBP; 79})$$

For open fuel types (O-1):

If  $WSV \geq 1.0$ :

$$LB = 1.1 + WSV^{0.464} \quad (\text{FBP}; 80)$$

If  $WSV < 1.0$ :

$$LB = 1.0 \quad (\text{FBP}; 81)$$

The lengths of A, B, C (Figure 1) are dependent on the distance between the source and target cells, and on LB. To calculate A, B, C we use components of the polar equation for an ellipse. First calculate the eccentricity (e).

$$e = \sqrt{1 - \left(\frac{1}{LB}\right)^2}$$

Next, calculate the semi-latus rectum (p), which is the distance from the focus to the ellipse perimeter perpendicular to the major axis.

$$p = dist \times (1 + e \times \cos(\pi - \beta))$$

where *dist* is the distance between the source cell center and the target cell center. Once p is calculated, we can calculate B and C.

$$B = \frac{p}{1 - e^2}$$

$$C = e \times B$$

B + C is the distance the fire would travel in the downwind direction from the rear focus of the ellipse. Given the rate of spread in the downwind direction ( $ROS_i$ ) calculated above, we can calculate the time it would take to travel a distance of B + C.

$$time = \frac{B + C}{ROS}$$

We know the distance that the fire must travel in the direction of the source cell (*dist*), and the time it should take to travel that distance (*time*), so we can calculate the average rate of spread in that direction (*DirROS*).

$$DirROS = \frac{dist}{time}$$

Take the inverse of *DirROS* to estimate the spread time “cost” in minutes per meter in that cell.

### 1.5.2. Fire Burned Area: Complex Time Cost Surface

The direction of travel for a fire front changes in response to heterogeneous fuels and topography and the presence of non-forested (barrier) cells. Therefore, we developed an algorithm that accounts for the length of the path required for fire to spread to each cell.

For each cell within the defined maximum distance (circle or ellipse), the algorithm searches for the neighbor with the shortest travel time. For the eight cells surrounding the ignition point, this shortest travel time will be zero. The neighbor travel time is added to

the travel time ( $1/\text{AdjROS}$ , above) calculated for each cell. The travel time is also adjusted to account for the cell size and relative distance from the neighbor to the cell (multiplied by  $[1.0 * \text{cell size}]$  for adjacent cells,  $[\sim 1.4 * \text{cell size}]$  for diagonal neighbors).

This neighborhood distance calculation is made once when the cells are recursively added during spreading. The travel times for each cell are checked for potentially shorter travel routes by iteratively searching for valid neighbors with shorter travel times. The list is searched up to 2000 times for shorter routes.

Once minimum travel time has been calculated for each site, the predetermined fire size or duration is used to identify which sites are included in the burned area. For size-based regimes, cells are added to the burn area in order of increasing time cost until the predetermined fire size is reached. For duration-based fires, all sites with a minimum travel time that is less than or equal to the predetermined fire duration are selected to become the burned area for that individual fire event.

## 1.6. Non-Forest Fuel Types

Active sites may include non-forested sites that will burn. Key examples include grassland, shrubland, and some wetland cover types that have establishment coefficients of zero (0) for all tree species. These active, non-forest sites can be defined in the FireEcoregions input table for the Dynamic Fire extension. User input fuel types can then be assigned to non-forested fire regions. For instance, grassland fire regions can be assigned an open-fuel type and shrubland fire regions may be compatible with a deciduous fuel type. These fuel types may be subject to additional seasonal parameters. If a fire region is not used in this extension, or if the user does not assign a fuel type to a non-forested fire region, the active sites within those fire regions will not be assigned to a fuel type and will not burn.

## 1.7. Topography (Optional)

Topography influences spread rates in a similar way as wind, so the effects of topography on spread can be modeled as wind factors. If the topographic effects option is turned on, the following equations calculate initial spread rates with slope influence (ISF) which substitutes for ISI in the above rate of spread equations.

Topographic effects on fire spread rates are based on the equation from Van Wagner (1977):

$$SF = e^{3.533 \times \left(\frac{GS}{100}\right)^{1.2}} \quad (\text{FBP}; 39)$$

where SF is the topography spread factor, and GS is the ground slope in percent. Note that the above equation is not recommended to apply to slopes greater than 60%.

First calculate the zero wind rate of spread (RSZ) within all cells falling within the Maximum Fire Event Region, using the above ISI equations, a wind speed of 0 km/hr, the FFMC, and the fuel type present on the cell (Forestry Canada Fire Danger Group 1992). The slope factor is then multiplied by this value to derive the “slope-adjusted zero wind rate of spread” (RSF):

$$RSF = RSZ \times SF \quad (\text{FBP; 40})$$

Next calculate the ISI with slope influence and zero wind:

$$ISF = \frac{\ln \left[ 1 - \left( \frac{RSF}{a} \right)^{\frac{1}{c}} \right]}{-b} \quad (\text{FBP; 41})$$

where a, b, c are fuel-type-specific rate of spread equation constants.

Equation FBP 41 will not work for two fuel type groups: mixedwood (M-1 and M-2) and grass (O-1). For fuel types M-1 and M-2:

$$ISF = \frac{\ln \left[ 1 - \left( \frac{100 - RSF}{PC \times a} \right)^{\frac{1}{c}} \right]}{-b} \quad (\text{FBP; 42})$$

where a,b,and c are fuel-type specific rates of spread for the softwood (C-2) component, and PC is percent conifer composition. For the O-1 fuel type:

$$ISF = \frac{\ln \left[ 1 - \left( \frac{100 - RSF}{CF \times a} \right)^{\frac{1}{c}} \right]}{-b} \quad (\text{FBP; 43})$$

where CF = the percent cured/dead material factor from FBP Eq. 35.

Next compute the slope equivalent wind speed (WSE):

$$WSE = \frac{\ln \left[ \frac{ISF}{0.208 \times f(F)} \right]}{0.05039} \quad (\text{FBP; 44})$$

where  $f(F)$  is the fuel moisture effect (see Section 1.3.5.; FBP 45, 46). WSE is the effect the percent slope would have on the rate of spread if it were a wind speed. This effect can be added to the wind speed along a transect between cell points by calculating percent slope from the difference in elevation between the cell points, adjusting the distance calculation to account for elevation change, calculating WSE using the equations in this section, using vector addition to combine the wind and slope effects, and then calculating rate of spread and travel time.

The vector addition uses the following equations:

$$WSX = [WS * \sin(WAZ)] + [WSE * \sin(SAZ)] \quad (\text{FBP; 47})$$

$$WSY = [WS * \cos(WAZ)] + [WSE * \cos(SAZ)] \quad (\text{FBP; 48})$$

$$WSV = \sqrt{(WSX^2 + WSY^2)} \quad (\text{FBP; 49})$$

$$RAZ = \arccos (WSY/WSV) \quad (\text{FBP; 50})$$

---

If  $WSX < 0$ , then  $RAZ = 360 - RAZ$  (FBP; 51)

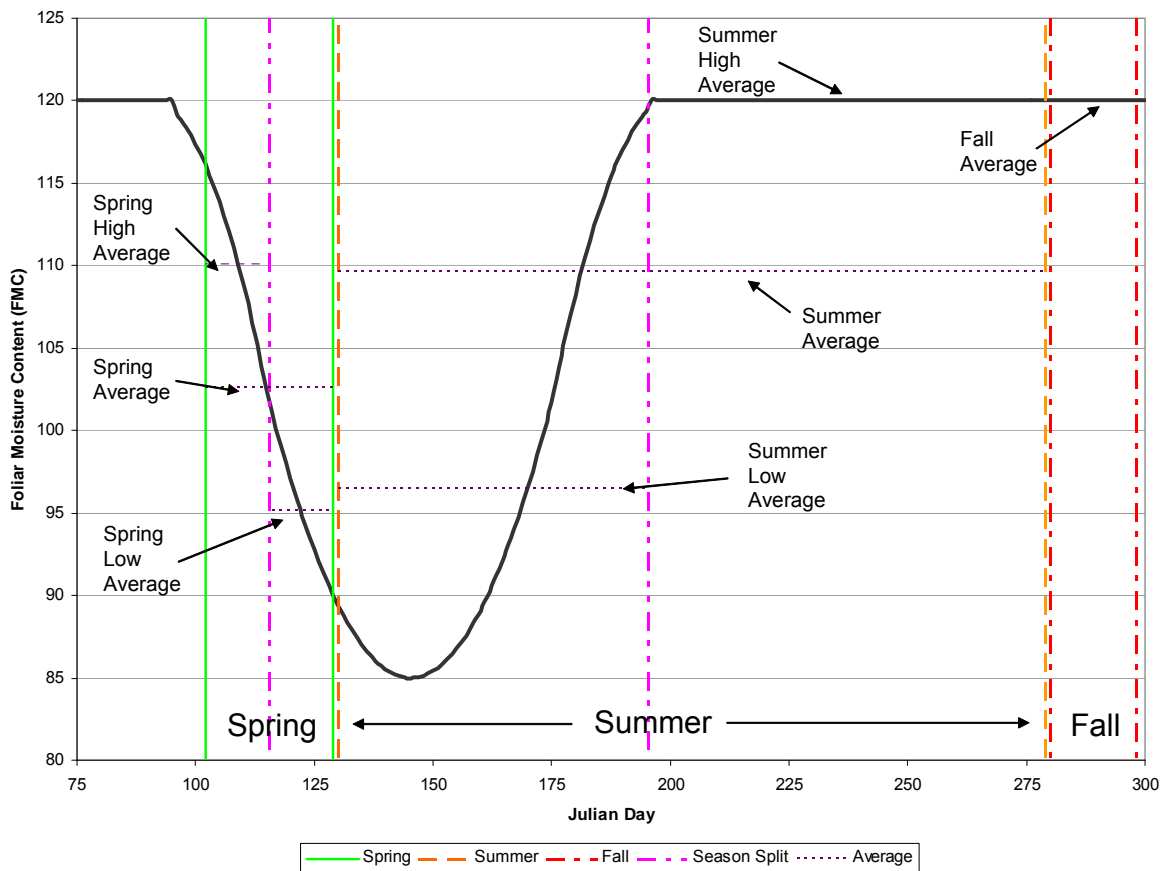
where WS is wind speed velocity, WAZ is the wind azimuth, SAZ is the uphill slope azimuth, WSV is the net effective wind speed, and RAZ is the net effective wind direction. This net effective wind speed and direction is then used for all subsequent calculations involving a wind speed or direction, including ISI and LB.

## 1.8. Fire Severity

At each site, a fire event will have a unique severity that is a user-defined function of the rate of spread (ROS) and the critical surface fire rate of spread (RSO), above which fires begin to reach the crown. Both affect fire intensity.

Crown Base Height (CBH) and foliar moisture code (FMC) are used to calculate the Critical Surface fire Intensity (CSI). CBH is defined by the user for each fuel type. FMC is dependent on location (lat/long), elevation, and Julian date. This value is defined by the user for each season by landtype, in the landtype table. The user can define 2 FMC values for each season, since phenology-based seasons do not necessarily coincide with the seasonality of FMC. This requires the user to define what proportion of fires within the landtype should be associated with each of the sub-season values. The user can choose to not divide the seasons by making one of the proportions equal to 1.0. See Figure 2 for an example of the seasonality of FMC and its relationship to phenology-based seasons.

Figure 2. Foliar moisture code (FMC) seasonality and corresponding phenology-based seasons.



Next, the Crown Fraction Burned (CFB) is calculated:

$$CSI = 0.001 * CBH^{1.5} * (460 + 25.9 * FMC)^{1.5} \quad (FBP;56)$$

$$RSO = CSI / (300 * SFC) \quad (FBP;57)$$

$$CFB = 1 - e^{(-0.23 * (ROS - RSO))} \quad (FBP;58)$$

Where Surface Fuel Consumption (SFC) is calculated using the following equations for each fuel type.

For C-1:

$$SFC = 1.5 * (1 - e^{(-0.2230 * [FFMC - 81])}), \quad (FBP;9)$$

if  $SFC < 0$ , then set  $SFC = 0$

For C-2, M-3, M-4:

$$SFC = 5.0 * (1 - e^{(-0.0115 * BUI)}) \quad (FBP;10)$$

For C-3, C-4:

$$SFC = 5.0 * (1 - e^{(-0.0164 * BUI)})^{2.24} \quad (FBP;11)$$

For C-5, C-6:

$$SFC = 5.0 * (1 - e^{(-0.0149 * BUI)})^{2.48} \quad (FBP;12)$$

For C-7, forest floor consumption (FFC) and woody fuel consumption (WFC) are calculated separately, and summed to get SFC:

$$\text{FFC} = 2 * (1 - e^{(-0.104 * (\text{FFMC} - 70))}) \quad , \quad (\text{FBP};13)$$

If FFC < 0, then set FFC = 0

$$\text{WFC} = 1.5 * (1 - e^{(-0.0201 * \text{BUI})}) \quad (\text{FBP};14)$$

$$\text{SFC} = \text{FFC} + \text{WFC} \quad (\text{FBP};15)$$

For D-1:

$$\text{SFC} = 1.5 * (1 - e^{(-0.0183 * \text{BUI})}) \quad (\text{FBP};16)$$

For Mixed fuel types (percent hardwood greater than zero):

$$\text{SFC} = (\text{PC}/100 * (\text{SFC for C-2 through C-7})) + (\text{PH}/100 * (\text{SFC for D-1})) \quad (\text{FBP};17)$$

For O-1:

$$\text{SFC} = \text{GFL} \quad (\text{FBP};18)$$

Grass fuel load (GFL) has a standard value of 0.3 kg/m<sup>2</sup>

For S-1:

$$\text{FFC} = 4.0 * (1 - e^{(-0.025 * \text{BUI})}) \quad (\text{FBP};19)$$

$$\text{WFC} = 4.0 * (1 - e^{(-0.034 * \text{BUI})}) \quad (\text{FBP};20)$$

For S-2:

$$\text{FFC} = 10.0 * (1 - e^{(-0.013 * \text{BUI})}) \quad (\text{FBP};21)$$

$$\text{WFC} = 6.0 * (1 - e^{(-0.060 * \text{BUI})}) \quad (\text{FBP};22)$$

For S-3:

$$\text{FFC} = 12.0 * (1 - e^{(-0.0166 * \text{BUI})}) \quad (\text{FBP};23)$$

$$\text{WFC} = 20.0 * (1 - e^{(-0.0210 * \text{BUI})}) \quad (\text{FBP};24)$$

For S-1, S-2, S-3:

$$\text{SFC} = \text{FFC} + \text{WFC} \quad (\text{FBP};25)$$

Finally, the fire severity is defined by the crown fraction burned (CFB), ROS, and RSO. An index of 1-5 is calculated, with 1 being the least severe and 5 being the most severe:

Class 5 has CFB >= 0.9

Class 4 has 0.495 <= CFB < 0.9

Class 3 has 0.1 <= CFB < 0.495.

Classes 1 and 2 both have CFB < 0.1.

Class 2 has a ROS >= (RSO + 0.458) / 2.

Class 1 has a ROS < (RSO + 0.458) / 2.

The Class 1 and 2 threshold value is based on calculating the ROS value required to have  $CFB = 0.1$  (this is when  $ROS = RSO + 0.458$ ). Then this range of ROS is divided evenly into the 2 classes.

## 1.9. Fire Damage

If fire severity = 5, then all cohorts of all species will be killed. If fire severity < 5, then fire damage is dependent upon the age of the cohorts at each site within an event and the fire tolerance of each species. The youngest cohorts are most vulnerable. For each cohort, the difference between the fire severity and fire tolerance is calculated. The difference determines which cohorts are killed; all cohorts below a User input relative age will be killed.

Table 1. Example of cohort age and the fire severity-fire tolerance differential. The values below were used in all previous LANDIS versions.

<b>Cohort Ages Killed</b> (% of species longevity)	<b>Severity – Species Fire Tolerance Differential</b>
≤ 20%	-2
≤ 50%	-1
≤ 85%	0
≤ 100%	1

Each fire event has an associated mean fire severity which is the average of the severities at all of the event's sites.

## 1.10. References

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## 1.11. Acknowledgments

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## 2. Parameter Input File

Most of the input parameters for this extension are specified in one input file. This text file must comply with the general format requirements described in section 3.1 *Text Input Files* in the *LANDIS-II Model User Guide*.

### 2.1. LandisData

This parameter's value must be "Dynamic Fire System".

### 2.2. Timestep

This parameter is the extension's timestep. Value: integer > 0. Units: years.

### 2.3. Event Size Type

Must be either 'size\_based' or 'duration\_based'.

### 2.4. Build Up Index

The Build Up index is either turned on or off. Values of 'Y' or 'yes' turn BUI on, and 'N' or 'no' turns BUI off. Having BUI turned off means BE will always be 1.0 and therefore not impact spread rates.

### 2.5. WeatherRandomizer (Optional)

The weather randomizer controls the strength of the linkage between the size/duration distribution and the weather distribution. This parameter is optional, with the default being a full-strength linkage, equivalent to a parameter value of 0. A full strength linkage means that the weather record will always be chosen from the same bin (1-5) as the size/duration bin. Values greater than 0 for this parameter allow the weather record to be selected from bins surrounding the selected size/duration bin. The weather record can then be selected from bins in the range (SizeBin  $\pm$  value). A parameter value of 4 means that there is no link between the size/duration and the weather data.

Value:  $0 \leq \text{integer} \leq 4$ .

### 2.6. Tables of Fire Region-dependent Parameters

The input file has a table of fire region-dependent parameters. Each row in a table contains the parameters for one fire region.

### 2.6.1. Fire Region Code

The first column in the table contains fire region map codes. The values must match the map values in InitialFireEcoregionsMap (2.7) and any maps listed in the DynamicEcoregionTable. Any map value that is not listed in this table will be assigned the default value of zero for all parameters.

### 2.6.2. Fire region Name

The second column in the table contains fire region names.

### 2.6.3. Mu

This parameter defines the location parameter of the lognormal distribution of fire sizes/durations for the fire region. This value is equivalent to the mean of the associated normal distribution. Expected mean for the lognormal distribution can be calculated as:  $e^{(\mu + \sigma^2)/2}$

Value: number  $\geq 0$ . Units: hectares or minutes.

### 2.6.4. Sigma

This parameter defines the scale parameter of the lognormal distribution of the fire sizes/durations for the fire region. This value is equivalent to the standard deviation of the associated normal distribution. Expected standard deviation for the lognormal distribution can be calculated as:  $\sqrt{(e^{\sigma^2} - 1) * e^{2\mu + \sigma^2}}$

Value: number  $\geq 0$  Units: hectares or minutes.

### 2.6.5. Maximum Size/Duration

This parameter defines the maximum size or duration that can be selected from the lognormal distribution. If a value higher than the maximum is selected, another value will be selected until one that is less than or equal to the maximum is chosen. Users who do not wish to truncate the lognormal distribution can set the maximum value to be extremely high relative to expected values.

### 2.6.6. Spring FMC Low

Foliar moisture content for the portion of the spring season with lower values.

Value:  $0 \leq$  number. Units: %

### 2.6.7. Spring FMC High

Foliar moisture content for the portion of the spring season with higher values.

Value:  $0 \leq$  number. Units: %

### 2.6.8. Spring High Proportion

The proportion of fires within the spring season that occur during the “high” FMC period. Spring Low Proportion is calculated as  $1.0 - \text{Spring High Proportion}$ .

Value:  $0.00 \leq \text{number} \leq 1.00$  Units: Proportion

### 2.6.9. Summer FMC Low

Foliar moisture content for the portion of the summer season with lower values.

Value:  $0 \leq \text{number}$ . Units: %

### 2.6.10. Summer FMC High

Foliar moisture content for the portion of the summer season with higher values.

Value:  $0 \leq \text{number}$ . Units: %

### 2.6.11. Summer High Proportion

The proportion of fires within the summer season that occur during the “high” FMC period. Summer Low Proportion is calculated as  $1.0 - \text{Summer High Proportion}$ .

Value:  $0.00 \leq \text{number} \leq 1.00$  Units: Proportion

### 2.6.12. Fall FMC Low

Foliar moisture content for the portion of the fall season with lower values.

Value:  $0 \leq \text{number}$ . Units: %

### 2.6.13. Fall FMC High

Foliar moisture content for the portion of the fall season with higher values.

Value:  $0 \leq \text{number}$ . Units: %

### 2.6.14. Fall High Proportion

The proportion of fires within the fall season that occur during the “high” FMC period. Fall Low Proportion is calculated as  $1.0 - \text{Fall High Proportion}$ .

Value:  $0.00 \leq \text{number} \leq 1.00$  Units: Proportion

### 2.6.15. Default Open Fuel Type Index

The index for the fuel type that will be used to calculate spread rates if no species-age cohorts are present on a cell within the fire region. The index value should match an index value from the Fuel Type Table (2.15).

Value:  $1 \leq \text{number} \leq n$  (number of fuel types) Units: Integer

### 2.6.16. Number of Fires

The number of fires expected per year within the fire region. This value is multiplied by the time step and used as  $\lambda$  for the Poisson distribution.

## 2.7. InitialFireEcoregionsMap

This parameter is the input map showing where the fire regions are located on the landscape. Each cell value must be one of the map codes listed in the fire fire regions table (2.5). This map can be the same as the succession ecoregions map.

## 2.8. DynamicEcoregionTable

This table enables the user to allow fire regions to change spatially through the course of a simulation. The first column represents the simulation time step (year) when the new map should be applied. The second column gives the filename of the new fire region map. The InitialFireEcoregionsMap will be applied until the time step reaches the first year listed in the table. The new map will be applied until the time step reaches the next year listed in the table. If no additional files are listed, the program will continue using the current fire region map. Use of the DynamicEcoregionTable is optional. If no additional maps are included in this table, the program will use the InitialFireEcoregionsMap for the entire simulation.

## 2.9. GroundSlopeFile (optional)

This optional parameter specifies a raster map to represent percent ground slope. The map should have integer values representing percent slope on the ground. If this map is included, the UphillSlopeAzimuthMap (2.10) must also be included.

## 2.10. UphillSlopeAzimuthMap (optional)

This optional parameter specifies a raster map to represent the direction of uphill slope. Values in this map should be integers ranging from 0 to 360 degrees, specifying the direction upslope. Note: this is the opposite of the way aspect is commonly defined. This parameter should only be specified if GroundSlopeFile (2.9) is specified, if which case this parameter is required.

## 2.11. Seasons Table

The seasons table must include an entry for each of the three seasons: spring leaf off, summer leaf-on, fall leaf-off. For each season, the following parameters must be provided:

parameter name	Units	description
Season Name	text	Names of the three seasons. Must be “Spring”, “Summer”, or “Fall”.
Leaf Status	text	Either “LeafOn” or “LeafOff”
Proportion	$0.0 \leq \text{double} \leq 1.0$	The proportion of fires that happen within each season
Percent Curing	$0 \leq \text{integer} \leq 100$	The degree of curing for grasses (%).
Daylength Proportion	$0.0 \leq \text{double} \leq 1.0$	The proportion of the 24-hour day that fires can actively spread. This parameter only affects duration-based simulations. Users who are using durations based on actual spreading times, rather than ignition to extinguishment times that span multiple days, may want to use a value of 1.0.

## 2.12. InitialWeatherDatabase

This parameter specifies the name of a comma-separated text file that contains the season weather data. The table should contain fields labeled:

“FFMC” (Fine Fuel Moisture Code)

“BUI” (Build-Up Index)

“WSV” (Wind Speed Velocity)

“WINDDir” (Wind Direction)

“FWIBin” (FWI class)

“Season”

“Ecoregion” (i.e., the fire region).

Season names (“Spring”, “Summer”, “Fall”) should be capitalized, and fire region names should match those listed in the fire region table (see 2.5) exactly (capitalization matters). Each row should represent a daily

record of weather data representative of the specified fire region. At least 1 record in each FWIBin (1-5) is required for any fire region-season combination that has a fire ignition rate (Section 2.6.1.5) greater than zero (e.g., a minimum of 5 records). If weather data are assumed to be the same for all fire regions, “All” can be used in the Fire region column to denote that weather records apply to all fire regions.

### 2.13. DynamicWeatherTable

This table enables the user to allow weather data to change through the course of a simulation. The first column represents the simulation time step (year) when the new weather data should be applied. The second column gives the filename of the new weather database. The InitialWeatherDatabase will be applied until the time step reaches the first year listed in the table. The new database will be applied until the time step reaches the next year listed in the table. The format and naming conventions of tables must be the same as described for the InitialWeatherDatabase (2.12). If no additional files are listed, the program will continue using the current weather database. Use of the DynamicWeatherTable is optional. If no additional files are included in this table, the program will use the InitialWeatherDatabase for the entire simulation.

### 2.14. Fuel Type Table

The fuel type table is mostly copied from Appendix 1 and Tables 6, 7 and 8 of the Canadian Forest Fire Behavior Prediction System (Forestry Canada Fire Danger Group 1992). The fuel type-specific ignition probability (second column) must be determined by the user. Standard values for all other values can be found in the FBP. These parameter values can be adjusted by the user to produce desired behavior, which may be particularly useful if the standard Canadian fuel types do not adequately model certain local fuel types. The fuel type table must have at least 1 entry each with a surface type of M1 and M2, though these types are not defined by the user in the fuel type definitions in the fuel extension. If using the BDA extension, or any other extension that produces dead conifers, the table must also include entries with surface types M3 and M4. These fuel types are required for initiation probability and severity calculations.

#### 2.14.1. Index

The first column in the table (Index), lists an integer index value for each fuel type. The index value in this table should correspond with index values used in the accompanying Fuel Extension. All index values that appear in the Fuel Extension need to be listed in this FuelTypeTable.

### 2.14.2. BaseType

All fuel types must be assigned to a base type, which can be Conifer, ConiferPlantation, Deciduous, Slash, or Open. The base type defines how the fuels are treated by the extension in calculations of fire spread, conifer dominance, and severity.

### 2.14.3. SurfaceType

All fuel types must be assigned to a fuel type on which to base surface fuel consumption (SFC) calculations. SFC is used in the calculation of fire severity, and uses fixed equations for each Canadian fuel type. Any custom fuel type needs to be assigned to a similar Canadian fuel type to allow calculation of SFC. Acceptable value for this parameter are C1-C7, D1, M1-M4, S1-S3, O1a, O1b.

## 2.15. Fire Damage Table

This table describes the fire damage classes. The values shown in the example file above were used in all previous LANDIS versions.

### 2.15.1. Table Name

The table's name is "FireDamageTable".

### 2.15.2. Cohort Age

This parameter is the upper bound of the range of cohort ages that a table row applies to. Values:  $0\% \leq \text{number} \leq 100\%$ . Units: Percentage of species' longevity.

### 2.15.3. Fire Severity – Fire Tolerance

This parameter is the minimum difference between the fire's severity and the species' fire tolerance in order for a cohort to be killed by a fire event. Value: integer.

## 2.16. MapNames

This file parameter is the template for the names of the fire severity output maps (see section 3.1). The parameter value must include the variable "timestep" to ensure that the maps have unique names (see Section 3.1.8.1 *Variables* in the *LANDIS-II Model User Guide*). **The user must indicate if the output should be placed in a sub-directory. Also, the user must indicate the file extension.**

## 2.17. LogFile

The file parameter is the name of the extension's event log file (see section 3.2).

## 2.18. SummaryLogFile

The file parameter is the name of the extension's summary log file for fire time steps (see section 3.3).

## 3. Output Files

The Dynamic Fire extension generates two types of output files: a) a map of fire severity for each time step, and b) two log files of fire events for the entire scenario.

### 3.1. Fire Severity Maps

The map of fire severity is labeled 0 for non-active sites, 1 for active and not disturbed sites, 2 for burned sites where no cohorts were damaged, and [fire severity + 2] for all disturbed sites. A map is produced for each fire time step.

### 3.2. Fire Event Log

The event log is a text file that contains information about every event over the course of the scenario: year, initiation cell coordinates, initiation fire region value, initiation fuel type, initiation percent conifer, selected size (**or duration**), actual duration, fire season, wind speed, wind direction, FFMC, BUI, % grass curing, number of damaged sites, number of cohorts killed total, mean fire severity across all sites, number of cells burned by fire region, and total fire size (number of cells). The information is stored as comma-separated values (CSV).

### 3.3. Fire Summary Log

The fire time step log is a text file that contains summary information about all the events that occurred during each fire time step: year, total number of cells burned, total number of cells burned by fire region, and total number of events,. The information is stored as comma-separated values (CSV).

**The first row (time step zero) indicates the total number of sites in an fire region.** These data are useful when calculating Fire Rotation Period (T/P where T is time in years and P is proportion burned including all burns, even those that spatially overlap).

## 4. Sample Input File

```

LandisData "Dynamic Fire System"

Timestep 10
>>EventSizeType      size_based <<or 'duration_based'
EventSizeType        duration_based <<or 'size_based'

BuildUpIndex  yes    << yes or no; Y or N
WeatherRandomizer 0 << optional (0 - 4)

>> Fire Sizes (parameters applied for both size and duration based)
>> EcoCode EcoName Mu Sigma Max SpFMCLo SpFMCHi SpHiProp SumFMCLo SumFMCHi SumHiProp
      FallFMCLo FallFMCHi FallHiProp OpenFuelIndex NumFires
>> -----
0  Water  0      0      0  120   120   1.0   120   120   1.00  120   120
   1.00  8  0
1  eco22  6.9    0.0031 50  91   108   0.09  98   120   0.02  120   120
   1.00  8  11
2  eco3   6.9    0.0031 50  91   108   0.09  98   120   0.02  120   120
   1.00  8  4.1
3  eco4   6.90   0.0031 50  90   107   0.09  99   120   0.02  120   120
   1.00  8  4.1

InitialFireEcoregionsMap  Fire_regions.gis
DynamicEcoregionTable
>>      Year      FileName
      20      Fire_regions20.gis

GroundSlopeFile          half_50_0.gis
UphillSlopeAzimuthMap    all_0.gis

SeasonTable
>>      Leaf      Proportion      Percent      DayLength
>> Name      status      Fire      Curing      Proportion
>> -----
Spring      LeafOff    0.07      0      1.0
Summer      LeafOn     0.93      51     1.0
Fall        LeafOff    0.00      100    1.0

InitialWeatherDatabase  FWI_Sample.mdb
DynamicWeatherTable
>>      Year      FileName
      20      FWI_sample_20.mdb

FuelTypeTable
>> Fuel Input Table
>> Index  Base      Surface IgnProb      a      b      c      BUI      maxBE  CBH
>>      Type      Type
1  Conifer  C1      1.0  90   0.0649 4.5   0.90  72   1.076  2
2  Conifer  C2      1.0  110  0.0282 1.5   0.70  64   1.321  3
3  Conifer  C3      1.0  110  0.0444 3.0   0.75  62   1.261  8
4  Conifer  C4      1.0  110  0.0293 1.5   0.80  66   1.184  4
5  Conifer  C5      1.0  30   0.0697 4.0   0.80  56   1.220  18
6  ConiferPlantation  C6      1.0  30   0.0800 3.0   0.80  62
   1.197  7
7  Conifer  C7      1.0  45   0.0305 2.0   0.85  106  1.134  10
8  Deciduous  D1     1.0  30   0.0232 1.6   0.90  32   1.179  0
9  Conifer  M1      1.0  0    0      0     0.80  50   1.250  0
10 Conifer  M2      1.0  0    0      0     0.80  50   1.250  6
11 Conifer  M3      1.0  0    0      0     0.80  50   1.250  6
12 Conifer  M4      1.0  0    0      0     0.80  50   1.250  6
13 Slash   S1      1.0  75   0.0297 1.3   0.75  38   1.460  0
14 Slash   S2      1.0  40   0.0438 1.7   0.75  63   1.256  0
    
```

15	Slash	S3	1.0	55	0.0829	3.2	0.75	31	1.590	0
16	Open	O1a	1.0	190	0.0310	1.4	1.0	01	1.000	0
17	Open	O1b	1.0	250	0.0350	1.7	1.0	01	1.000	0

SeverityCalibrationFactor 1.0

FireDamageTable

>> Cohort Age            FireSeverity -

>> % of longevity        FireTolerance

>> -----

20%	-2
50%	-1
85%	0
100%	1

MapNames fire/severity-{timestep}.gis

LogFile fire/log.csv

SummaryLogFile fire/summary-log.csv

# LANDIS-II Dynamic Fuel System v1.0 Extension User Guide

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# 1 Introduction

This document describes the **Dynamic Fuel System** extension for the LANDIS-II model. For information about the model and its core concepts, see the *LANDIS-II Conceptual Model Description*.

The **Dynamic Fuel System** extension described herein uses species age, conifer mortality, and post disturbance information at each site to classify every active site into a season-independent fuel type. This extension will produce maps of fuel types, percent conifer, and percent dead fir. Assigning active sites to fuel types is a required input for the external **Dynamic Fire System** extension. Therefore, the Dynamic Fuel System is a disturbance extension and should be run immediately prior to the Dynamic Fire System within the scenario file.

## 1.1 Fuel Types

A fuel type can be defined as “an identifiable association of fuel elements of distinctive species, form, size, arrangement, and continuity that will exhibit characteristic fire behavior under defined burning conditions” (Merrill and Alexander 1987). For example, the Canadian Fire Prediction System fuel types are described qualitatively based on stand structure, composition, surface fuels, ladder fuels, and forest floor characteristics, including cover and duff (FBP; Forestry Canada Fire Danger Group 1992). The Canadian FBP System includes five major groups and 16 discrete fuel types (Appendix, Table 1).

The LANDIS-II **Dynamic Fuel System** extension (‘fuel extension’ henceforth) allows up to 100 different fuel types, limited to the following base fuel types: Conifer, ConiferPlantation (type C-6 in the Canadian FBP System), Deciduous, Slash, and Open. The rules defined below determine which fuel type each site is assigned. These types – each given a numeric index - must match the fuel types and indices defined in the **Dynamic Fire System** extension. If a site is assigned a fuel type that is not listed in the Dynamic Fire System extension, the default values will be zero and fire will be unable to spread and burn across that site.

## 1.2 Fuel Classification

The fuels classification is determined by where a cohort falls within a fuel type age range. The formula is:

$$SpeciesValue = \sum_0^n \frac{CohortAge - RangeMinimum}{RangeMaximum - RangeMinimum} \times SppCoefficient$$

where *CohortAge* is the age (years) of the oldest cohort of that species that falls between *RangeMaximum* and *RangeMinimum*; *RangeMaximum* is the maximum of the age range for a given fuel type; *RangeMinimum* is the minimum of the age range for the same fuel type; and *SppCoefficient* is a user specified weight (0 – 1.0) that can be assigned to each species (default = 0). For each species, *RangeMaximum* is truncated to the species longevity if it exceeds longevity.

For each fuel type, these species values are summed (or subtracted if given the negative switch, see below), depending upon which species are listed for the fuel type. The fuel type with the highest overall score is assigned to the cell.

The species coefficients provide flexibility in determining the influence of a particular species on fire spread rates for mixedwood fuel types, and is a user input value ( $0.0 \leq SppCoefficient \leq 1.0$ ). Species coefficients are generally recommended at or near 1.0 (the default value) for all species. For instance, a species coefficient value of 0.95 for a particular conifer species in a mixedwood type can substantially reduce conifer dominance (see below), giving more influence to the deciduous component on fire spread rates. If a deciduous species is assigned a *SppCoefficient* < 1.0, then the conifer component in a site with that species will have more influence on fire spread rates.

In order to accommodate mixed fuel types, a deciduous fuel type is also calculated based solely on the fuel types that are designated ‘Deciduous’ base type.

### 1.3 Conifer and Deciduous Dominance

Conifer and deciduous dominance (CD and DD, respectively) is used to determine if sites are initially assigned to either a coniferous, deciduous, or a mixed fuel type. The actual blending of a conifer type and a deciduous type to create a mixed type occurs within the Dynamic Fire System and the user need not create mixed types in the Dynamic Fire System.

The conifer dominance is calculated using the sum of dominance values for the two conifer base types (Conifer and ConiferPlantation). Deciduous dominance is the sum of dominance values for the Deciduous base type. To determine their respective types, each is divided by the sum of conifer plus deciduous dominance.

An optional, maximum percent hardwood (PH) “cut-off” value can be set that will determine whether sites containing both deciduous and coniferous species are treated as a single fuel or a mixed fuel type. The default maximum PH value

for placement of a site into the coniferous fuel group category is 0% (i.e.,  $CD = 1.0$ ). Under this default setting, active sites that contain both deciduous and coniferous species (i.e.,  $PH > 0\%$ ;  $CD < 1.0$ ) are treated as a mixed fuel types and fire spread rates will be calculated as a proportional blend of the deciduous and coniferous fuel types (see equations 27 & 28 in the **Dynamic Fire System** Users Guide). The PH can be adjusted such that an active site containing both coniferous and deciduous species being placed into either a coniferous or deciduous fuel type. This enables the user to prevent sites from being treated as a mixed fuels when either the deciduous or coniferous component is minor (e.g., a mature-conifer dominated site that contains one young-age cohort of a single deciduous species). The PH can also be used to categorize mixed sites as entirely deciduous (when  $CD > 100 - PH$ ). Therefore, if the PH value is  $> 0$ , mixed types occur only when CD is between PH and  $100 - PH$ . Caution should be used in setting the maximum PH value above the default value (zero), and interactions with the user-defined fuel coefficient set in the CD equation should be carefully considered and tested.

If the selected fuel type is either Slash or Open base fuel types, then both the conifer dominance and deciduous dominance are set to zero. If the selected fuel type is ConiferPlantation, then conifer dominance is set to 100 and deciduous dominance set to zero.

## 1.4 Dead Conifer Index

To reflect the ladder-fuel effects of dead conifers in a stand understory, the Dynamic Fuel System can apply an optional dead conifer index calculated from the **Base BDA** Extension. The dead conifer index is based on the total number of dead fir and spruce cohorts relative to the current total number of cohorts at each site, with possible values ranging from 0 to 100. An input duration determines how far back in simulation time to consider dead fir cohorts.

The dead conifer index input is applied to all mixed and conifer fuel types within the **Dynamic Fire System**. Any dead conifer index value  $> 0$  alters the spread rate for any Conifer, Conifer Plantation, and any mixed fuel types (depending on the fire season input in the Fire Extension). A conifer fuel type combined with dead conifer index  $> 0$  will be converted to the M-3 (dead balsam fir leaf off) fuel type in the Dynamic Fire System. The deciduous and mixed fuel types combined with a dead conifer index  $> 0$  can be converted to either M-3 or M-4 fuel types, dependent upon fire season. If the optional dead conifer index or the Base BDA Extension are not active, the Dynamic Fuel Extension will assign a default value of “no effect” for the dead conifer index.

## 1.5 Post Disturbance Information

To simulate the change in fuels following a disturbance, the fuels extension provides an option to assign an active site to a new fuel type. The user must also indicate the duration (in number of years) for the conversion fuel types. These new fuel types can be any fuel listed in the **Dynamic Fire System** extension. After a stipulated number of years expire, the conversion fuel type is replaced by a new fuel type, based on other fuel extension inputs and parameters.

The name of the disturbance can be one of three general options: 1) a Harvest prescription name, 2) a wind severity, or 3) a fire severity. The rules for giving fire and wind severity names are given below.

If a harvest prescription results in a slash types, remember that slash typically persists for only a few years after harvest. Unless fuels are arranged to occur after harvesting and with the same time step, this short time frame requires setting yearly time steps in the Dynamic Fuel System.

## 1.6 Acknowledgements

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## 2 Input File

The input parameters for this extension are specified in one input file. This text file must comply with the general format requirements described in section 3.1 *Text Input Files* in the *LANDIS-II Model User Guide*.

### 2.1 LandisData

This parameters value must be “Dynamic Fuel System”

### 2.2 Timestep

This parameter is the timestep of the wind extension. Value: integer > 0. Units: years.

### 2.3 Species Fuel Coefficients

This parameter is a list of tree species with user-assigned fuel coefficients for determining relative dominance as a fuel type. If a species is not listed the default value is one (1).

### 2.4 Hardwood Maximum

The optional Hardwood Maximum value determines the maximum percent (%) hardwood acceptable for a site to be placed into a coniferous fuel group and must be an integer between 1 and 100. If this parameter is not present, then the default value of zero (0) is used.

### 2.5 Dead Fir Maximum Age

The DeadFirMaxAge value determines the duration of influence for the dead conifer index produced by the BDA Extension. After this amount of time has passed since the last BDA event for each site, the dead conifer index for that site will be reset to 0.

### 2.6 Fuel Type Table

This suite of parameters defines the desired fuel type classification outputs and must be preceded by the keyword FuelTypes. The input is a table with user-defined fuel types, a base fuel category for each fuel type, the characteristic species for each fuel type, and the cohort age range for the characteristic species in each fuel type (Table 1).

Table 1.

Parameter	Data Type	Units	Example
Fuel Type Index	int		1
BaseFuel	string		Deciduous
Age range	{int} to {int}	years	0 to 40
Species	string		pinustro

The Fuel Type Index is an integer value that connects the fuel type to fuel parameters in the Fire Extension. The index values provided here should match index values included in the FuelTypeTable in the fire extension input file. All index values in the fuel input file must be included in the fire input file.

The BaseFuel category defines which fuel types are considered Conifer, ConiferPlanation, Deciduous, Open, or Slash. These categories are used in calculations of conifer dominance and for fire spread and severity calculations in the Fire Extension. The base fuel category identified for each fuel type here should match the base fuel category defined for the same fuel type in the Fire Extension FuelTypeTable input.

If a species should contribute to the dominance value of a fuel type, list the species name in the Species column. If a species should be subtracted from a fuel type, list the species name preceded by a '-' (negative) sign.

This table requires entries for fuel types within the coniferous, deciduous and open fuel groups. Descriptions for boreal mixedwood (M-1, M-2) and dead balsam fir mixedwood (M-3, M-4) fuel types are not entered into this table, as these are delineated differently, using conifer dominance and dead conifer index inputs, respectively. Unforested sites will have a default value of zero (0), unless a default fuel type is specified for the ecoregion in the Fire Extension.

## 2.7 Post Disturbance Fuel Information

This optional suite of parameters defines the conditions under which the fuel types are modified by other disturbances and must be preceded by the keyword DisturbanceConversionTable. The input is

fuel type index, the maximum duration (age in years) of each disturbance fuel type, and the exact name of the harvest prescription used in the Base Harvest Extension or disturbance type and severity class that will create that particular fuel type (Table 3). The fuel type index should correspond to fuel type indices included in the Fire Extension input file. The keywords FireSeverity and WindSeverity have been designated to cause fire and wind disturbances to change fuel types. Each keyword should be followed immediately (no space) by the severity class (1-5) of that disturbance to be used (e.g., FireSeverity3, WindSeverity4).

Table 3.

Parameter	Data Type	Units	Example
Fuel Type	integer		13
Duration	integer	years	3
Disturbance	string		JackPineClear WindSeverity4 FireSeverity2

## 2.8 Fuel Type Maps

The next parameter, MapFileNames, describes where the fuel type map is placed and its format. **This convention applies to all map names.** The first portion lists the directory where the maps should be placed relative to the location of the scenario text file (e.g., fire/). The parameter value “timestep” must be included and will be replaced with the output time step. Other characters can be inserted as desired. A meaningful file extension (e.g., .gis) should also be included.

**Fuel types are mapped as their index + 1. Non-active sites are given a value of zero.**

## 2.9 Percent Conifer Map Name

The next parameter, PctConiferMapName, describes where the percent conifer output maps are placed and their format. The first portion lists the directory where the maps should be placed relative to the location of the scenario text file (e.g., fire/). The parameter value “timestep”

must be included and will be replaced with the output time step. Other characters can be inserted as desired. A meaningful file extension (e.g., .gis) should also be included.

## 2.10 Percent Dead Fir Map Name

The final parameter, PctDeadFirMapName, describes where the percent dead fir output maps are placed and their format. The first portion lists the directory where the maps should be placed relative to the location of the scenario text file (e.g., fire/). The parameter value “timestep” must be included and will be replaced with the output time step. Other characters can be inserted as desired. A meaningful file extension (e.g., .gis) should also be included.

### 3 Example File

```

LandisData "Dynamic Fuel System"

Timestep 10

>> Fuel
>> Species Coefficient
>> -----
    betupapy    0.90
    piceglau    0.95

>> Optional Percent Hardwood Value (%)
HardwoodMaximum 10

DeadFirMaxAge 15

FuelTypes
>> Fuel Type      BaseFuel   Age Range      Species
>> -----
    2              Conifer    0 to 400      piceglau abiebals
    3              Conifer    0 to 40       pinubank
    4              Conifer    41 to 100     pinubank
    5              Conifer    100 to 400    pinustro pinuresi -abiebals
    6              ConiferPlantation 10 to 100    pinustro pinuresi
    16             Open      0 to 10       pinustro pinuresi
    8              Deciduous  0 to 1000     betupapy

HarvestConversionTable
>> SlashType      Duration   Prescription (more than one allowed)
>> -----
    13             5         JackPineClearCut
    14             15        WhiteSpruceHarvest

MapFileNames      fire/FuelType-{timestep}.gis
PctConiferMapFileName fire/PctConifer-{timestep}.gis
PctDeadFirMapFileName fire/PctDeadFir-{timestep}.gis

```

## 4 Appendix

Table 1. Canadian FBP System fuel types. For a complete description of each type, refer to Canadian Forest Fire Behavior Prediction System (Forestry Canada Fire Danger Group 1992) These fuel type are **not required**.

Group/Identifier	Descriptive name
Coniferous	
C-1	Spruce-lichen woodland
C-2	Boreal spruce
C-3	Mature jack or lodgepole pine
C-4	Immature jack or lodgepole pine
C-5	Red and white pine
C-6	Coniferous plantation
C-7	Ponderosa pine-Douglas-fir
Deciduous	
D-1	Leafless aspen
Mixedwood	
M-1	Boreal mixedwood-leafless
M-2	Boreal mixedwood-green
M-3	Dead balsam fir mixedwood-leafless
M-4	Dead balsam fir mixedwood-green
Slash	
S-1	Jack or lodgepole pine slash
S-2	White spruce-balsam slash
S-3	Coastal cedar-hemlock-Douglas-fir slash
Open	
O-1	Grass